

# Status Report

## Potential and Costs for Control of NO<sub>x</sub> Emissions in Europe

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SR-89-1  
November 1989



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### **Abstract**

The various technological options for reducing emissions of  $\text{NO}_x$  from stationary sources (powerplants) and mobile sources (four-stroke gasoline engines, light and heavy-duty diesel engines) are reviewed. A framework for developing the cost estimates of these options, based upon the free exchange of control technology in Europe, is developed. Both technology-specific and country-specific parameters are used. The cost estimates for various options applied to the different stationary and mobile sources in each country can be ranked in order of cost-effectiveness to generate National Cost Curves for  $\text{NO}_x$  control in each country. These cost curves can then be used by the IIASA Regional Acidification Information and Simulation (RAINS) model to estimate the costs of various scenarios including the currently committed emission reductions and the application of best available technology. In the future, they will also be used to develop cost-optimal emission control strategies for nitrogen oxides in Europe.

### **Acknowledgements**

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# Contents

<b>1</b>	<b>Introduction</b>	<b>3</b>
<b>2</b>	<b>Emissions of nitrogen oxides</b>	<b>5</b>
2.1	Emission mechanisms . . . . .	5
2.2	Emission inventories . . . . .	6
<b>3</b>	<b>Control of nitrogen oxides emissions</b>	<b>10</b>
3.1	Stationary sources . . . . .	11
3.1.1	Combustion modification . . . . .	11
3.1.2	Flue gas cleaning . . . . .	12
3.2	Mobile sources . . . . .	15
3.2.1	NO <sub>x</sub> control for Otto engines . . . . .	15
3.2.2	Diesel engines . . . . .	18
3.3	NO <sub>x</sub> control options selected for cost evaluation . . . . .	21
3.3.1	Stationary sources . . . . .	21
3.3.2	Mobile sources . . . . .	23
<b>4</b>	<b>Costs of NO<sub>x</sub> abatement</b>	<b>26</b>
4.1	Principles of cost calculation . . . . .	26
4.1.1	International consistency . . . . .	27
4.1.2	Benefits of NO <sub>x</sub> control . . . . .	28
4.2	Economic method . . . . .	29

4.3	Stationary sources . . . . .	30
4.3.1	The algorithm for the cost evaluation . . . . .	30
4.3.2	Data for cost calculation . . . . .	34
4.4	Mobile sources . . . . .	41
4.4.1	The algorithm for the cost evaluation . . . . .	41
4.4.2	Data for cost calculation . . . . .	42
4.5	Cost coefficients for NO <sub>x</sub> abatment . . . . .	45
4.6	National cost curves for NO <sub>x</sub> abatement . . . . .	47
4.7	Current reduction plans and maximum feasible reductions . .	49
<b>5</b>	<b>Conclusions</b>	<b>54</b>
	<b>References</b>	<b>56</b>
	<b>Appendix: National cost curves for NO<sub>x</sub> abatement</b>	<b>60</b>

# Chapter 1

## Introduction

The Regional Acidification Information and Simulation (RAINS) model developed at IIASA combines information on several stages of the acidification processes in the environment: the sources of emissions and the potential for their abatement, the transport of air pollutants in the atmosphere and the environmental effects of acid deposition. These impacts are evaluated on a regional scale for the whole of Europe for forest stands, forest soils and lakes (Alcamo *et al.*, 1987). In doing so, the model includes the pathways of the main precursors of acidification  $\text{SO}_2$ ,  $\text{NO}_x$  and  $\text{NH}_3$  (Figure 1.1).

Since the RAINS model is designed as a tool for assessing the efficiency of different pollution control strategies and their environmental effects, the analysis of removal potential and control costs for different abatement strategies forms an essential part within the whole procedure. Cost functions for the control of  $\text{SO}_2$  emissions have already been developed (Amann and Kornai, 1987). Therefore, the scope of this paper deals with the potential and the expected costs for abatement of  $\text{NO}_x$  emissions in Europe.

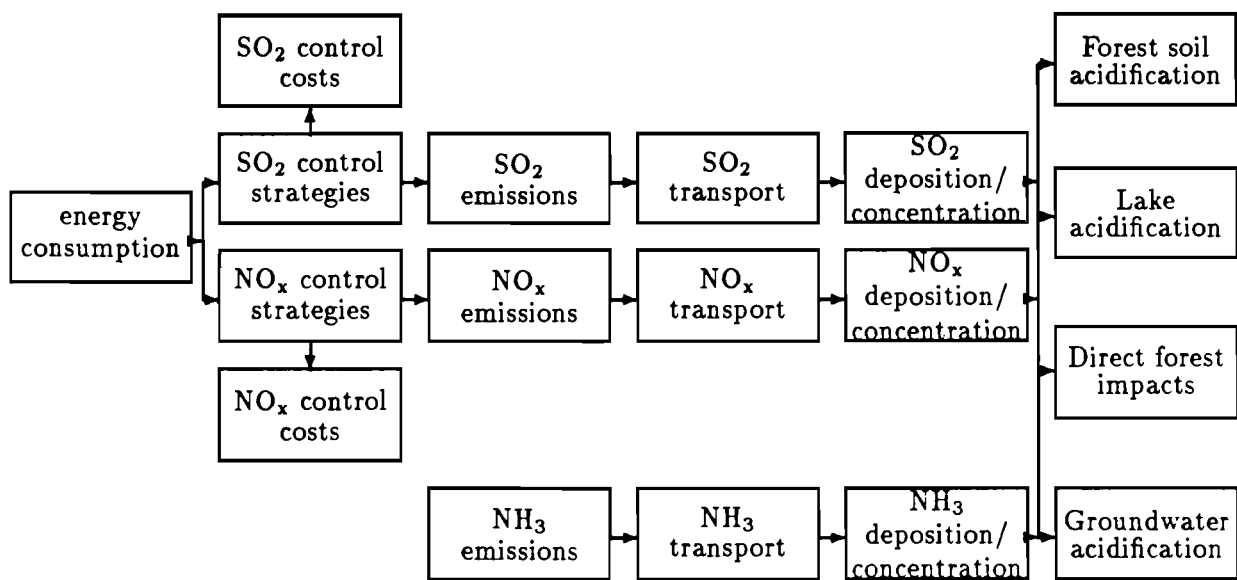


Figure 1.1: Structure of the RAINS model



## Chapter 2

# Emissions of nitrogen oxides

### 2.1 Emission mechanisms

Anthropogenic  $\text{NO}_x$  emissions originate mostly from energy combustion in stationary and mobile sources. Emissions from industrial processes (not associated with fuel combustion, e.g. the production of nitric acid) have only minor importance in Europe (Springmann, 1989). Two chemical reactions appear as the most important formation mechanisms for nitrogen oxides during the combustion of fossil fuels:

**Fuel  $\text{NO}_x$ .** During combustion the nitrogen chemically associated with the fuel (as apart from the molecular nitrogen which is part e.g. of natural gas) converts to amines and cyanids, which then together combine with oxygen to form nitrogen oxides. This 'fuel  $\text{NO}_x$ ' formation is a function of the fuel's nitrogen content as well as of the burner type and firing mode that is used. Fuel nitrogen contents typically vary for coal between 0.5 and 2.0 percent (by weight), and are less than 1 percent for oil. In natural gas the nitrogen content is negligible (U.S. Department for Energy, 1983). Because of the simultaneous reverse reaction (i.e. formation of nitrogen from nitrogen oxides), typically

only between 5 and 25 percent of the total fuel nitrogen is converted to  $\text{NO}_x$ .

**Thermal  $\text{NO}_x$ .** The thermal  $\text{NO}_x$  generation is due to the mechanism discovered by Zeldovich, in which nitrogen and oxygen from the air combine to form  $\text{NO}_x$  under high temperature (Equations 2.1 and 2.2).



This formation process usually becomes important at temperatures above 1400 degrees C (Rentz, 1984), a temperature which is generally exceeded in most combustion processes. At higher temperatures, thermal  $\text{NO}_x$  generation increases exponentially. It also depends on the residence time of combustion air in the combustion chamber and the availability of excess air.

The largest fraction of nitrogen oxides emissions are emitted as NO (monoxide) and are oxidized in the atmosphere to  $\text{NO}_2$  (dioxide). Recently greater attention has also been drawn to the generation of  $\text{N}_2\text{O}$  because of its contribution to the global greenhouse effect. For purposes of bookkeeping for emission estimates, however, all species of nitrogen oxides are usually converted to  $\text{NO}_2$ .

## 2.2 Emission inventories

During recent years several emission inventories have described the status of  $\text{NO}_x$  release for single European countries or for regions of Europe (e.g. Lübker *et al.*, 1989; Pacyna, 1989; Larssen, 1989). However, up to now there has been only a limited international consistency of these estimates: Some of these efforts put emphasis on converting official national data into

a common data format (e.g. the OECD-MAP emission inventory), but did not check the accuracy of the underlying emission calculations (e.g. the reasonableness of the emission factors in use). Other inventories have developed estimates based on internationally consistent sets of emission factors for some countries, but due to the limited availability of data they do not cover all of Europe.

Therefore, for the RAINS model a simplified approach was developed for calculating national NO<sub>x</sub> emissions for all 27 European countries based on a common set of energy consumption and emission data. The energy data cover the time period from 1960 to the year 2000 with forecasts based on official data (Amann, 1989). These data are disaggregated into 6 economic sectors and 12 fuel types. In order to enable a reasonable accuracy of the NO<sub>x</sub> emission estimates, additional breakdowns describe for each country the shares of wet bottom and dry bottom boilers in the coal powerplant sector and the fraction of two-stroke engines within the gasoline fueled car fleets.

The NO<sub>x</sub> emission factors (describing the emission characteristics for individual combustion processes) are considered as technology-specific and are therefore assumed equal for all countries (Table 2.1). This approach enables us to reconstruct emission figures to values within reasonable ranges of those officially submitted to international organizations (Table 2.2).

Table 2.1: NO<sub>x</sub> emissions factors (in g NO<sub>2</sub>/GJ fuel use)

<i>Fuel</i>	<i>Sector</i>				
	Con- version	Power- plants	Do- mestic	Trans- port	Indus- try
Brown Coal	200	270	70	n.a.	200
Hard Coal	230	1)	80	n.a.	230
Derived Coal	230	n.a.	70	n.a.	230
Middle Distillates	70	n.a.	70	2)	70
Heavy Fuel Oil	170	200	160	n.a.	170
Gasoline	70	n.a.	n.a.	3)	70
Natural Gas	0	150	60	n.a.	70
Other Solids	130	n.a.	60	n.a.	130

*Notes:*

- 1) Hard Coal, Dry bottom boiler 300  
Hard Coal, Wet bottom boiler 420
- 2) Diesel, Passenger Cars  
and Light Duty Trucks 350  
Diesel, Heavy Duty Trucks 1300
- 3) Gasoline, 4-stroke engines 750  
Gasoline, 2-stroke engines 160

Source: Springmann (1989)

Table 2.2: NO<sub>x</sub> emissions in 1980 (in kt NO<sub>2</sub>). Sources: Springmann (1989); UN-ECE (1988b); OECD (1989a)

Country	RAINS	ECE	OECD
Albania	28	9	-
Austria	239	216	216
Belgium	439	442	336
Bulgaria	357	150	-
CSSR	796	1204	-
Denmark	250	247	245
Finland	234	280	278
France	1944	2560	1962
FRG	2891	2950	2936
GDR	850	965	-
Greece	239	127	217
Hungary	305	270	-
Ireland	89	67	75
Italy	1458	1480	1599
Luxembourg	31	23	23
Netherlands	577	548	551
Norway	169	181	185
Poland	1597	1500	-
Portugal	149	166	165
Romania	661	390	-
Spain	950	950	937
Sweden	333	318	318
Switzerland	186	196	205
Turkey	356	175	-
UK	2324	1916	1924
USSR	9454	2790	-
Yugoslavia	394	190	-
Total	27317	20310	-

## Chapter 3

# Control of nitrogen oxides emissions

Emissions of nitrogen oxides can be controlled by several means:

- **Lower consumption of fuels that lead to high NO<sub>x</sub> emissions.**  
The consumption of energy can be reduced (i) through a lower final demand for energy services on the consumer side, (ii) by an increased combustion efficiency and (iii) substitution of fuels that lead to high NO<sub>x</sub> emissions by other energy forms. However, in some cases an increase in fuel efficiency may lead to higher NO<sub>x</sub> emissions (e.g. in the transportation sector).
- The control of nitrogen oxides generation during combustion through **combustion modification** techniques;
- and the removal after combustion by **flue gas cleaning** devices.

For this study, the options for emission reductions by structural changes of the energy system were excluded. A thorough analysis of the potential for and the macroeconomic impacts of structural changes to the energy system

would require detailed national models that are well beyond the present approach of the RAINS model. Such studies have already been undertaken by several researchers, but due to the complexity of the issue have focused only on a limited number of countries (e.g. Klaassen *et al.*, 1988; Rentz, 1984; Bergman *et al.*, 1988). Consequently, this study puts the emphasis on an internationally consistent assessment of direct control measures, applicable to existing energy infrastructures without major restructuring processes.

### **3.1 Stationary sources**

#### **3.1.1 Combustion modification**

During recent years improvements in the boiler design have resulted in considerable reductions of NO<sub>x</sub> formation during the combustion processes. Although the level of NO<sub>x</sub> emissions from the same fuel varies considerably with the type of the plant (depending on design characteristics such as spacing of burners and fuel-to-air ratio) all combustion modification techniques make use of the same principles:

- the reduction of excess oxygen levels (especially at periods of peak temperature);
- reduction of the peak flame temperature.

There are several types of control systems, based on combustion modification, that are presently in commercial operation:

#### **Low-NO<sub>x</sub> burners**

Low-NO<sub>x</sub> Burners (LNB) rely on the adjustment of the flame in the combustion process to reduce both thermal and fuel NO<sub>x</sub> formation. The advantages of LNB are ease of installation and the opportunity for retrofit in existing plants. In addition, LNB cause a minimum of energy loss from unburned

particles. The reductions of  $\text{NO}_x$  emissions through use of LNB are in the range of 30 to 50 percent.

#### **Off-stoichiometric combustion**

Off-stoichiometric combustion (OSC) regulates the oxygen content in the furnace to reduce primarily the formation of fuel  $\text{NO}_x$  and secondarily the formation of some of the thermal  $\text{NO}_x$  (e.g. by 'staged combustion'). While most of the installations have been in coal-fired units, there is now also some experience with natural gas plants. The effectiveness of OSC is site- and fuel specific but generally achieves reductions up to 30 percent; for natural gas plants somewhat higher percentages seem to be feasible.

#### **Flue gas recirculation**

Flue gas recirculation has been widely used in gas- and oil-fired utilities in the United States and can result in reductions of up to 45 percent for oil plants and from 50 to 70 percent for natural gas fired facilities.

#### **Catalytic combustion**

Catalytic combustion, uses a solid surface in the combustion vessel as a catalyst. This method is presently under development and shows a potential of some 80 percent reduction of  $\text{NO}_x$  and CO and an increase in the combustion efficiency of 1 - 2 percent. However, this technology is not yet commercially available.

### **3.1.2 Flue gas cleaning**

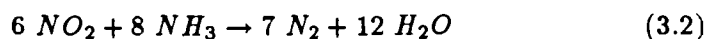
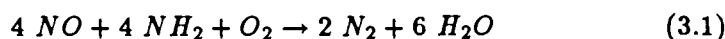
During recent years a variety of different flue gas treatment methods have been developed to remove  $\text{NO}_x$  after the combustion process. From the large number of available processes, the 'Selective Catalytic Reduction' (SCR) has



become the most important technique and is at present widely applied in some countries.

### **Selective catalytic reduction (SCR)**

The SCR process uses ammonia to convert nitrogen oxides into molecular nitrogen ( $N_2$ ) and water ( $H_2O$ ) in presence of a catalyst. The most important chemical reactions are:



Titanium oxide  $TiO_2$  is usually used as the catalytic material, but oxides of vanadium, molybden, tungsten, nickel and chromium are also in use. The major advantage of the SCR process is that it does not produce a by-product. The removal efficiency lies typically in the range between 80 and 90 percent and depends on the 'space velocity' (i.e. how quickly the exhaust gas stream moves through the catalysts) and on the amount of  $NH_3$  added. After some time in operation the activity of the catalysts declines, so that they have to be exchanged periodically. However, experience shows that the originally guaranteed lifetime of some 2 years is often significantly exceeded.

The operation of the conversion process is crucially related to a certain temperature range (e.g for catalysts of titanium oxides between 300 and 400 degree Celsius). Two most common design concepts are in use:

**High-dust System.** The SCR reactor is situated directly after the boiler before the electrostatic precipitator and any desulfurization device.

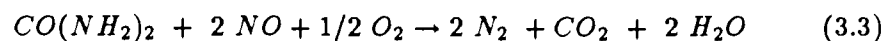
**Tail-Gas System.** The catalyst is located at the end of the flue gas path after the removal of dust and sulfur. This design principle results in higher life times of the catalysts, since they are operated with almost dust-free flue gas at low concentrations of  $SO_2$ . Therefore, the plants

can be designed independently of the fuel and boiler type, an advantage for retrofit applications. Any possible leaking of excess  $\text{NH}_3$  will not have impacts on installations downstream of the SCR reactor. On the other hand, in order to maintain the necessary temperature of the conversion process, a heat exchanger and reheating have to be provided.

Operating experience with SCR is rapidly growing. Most of the existing SCR plants are in Japan, but in the FRG a major retrofitting program of SCR is also close to completion. Due to the increasing experience the prices for catalysts are declining. On the West German market for example, the price per  $\text{m}^3$  of catalysts has shrunk from some 40.000 DM in 1985 to less than 20.000 DM today (Schärer and Haug, 1988).

#### Selective non-catalytic reduction

This technique controls  $\text{NO}_x$  by injection of ammonia or other reducing agents into the flue gas; the  $\text{NO}_x$  reduction takes place without use of a catalyst. The use of urea, for example, results in the following chemical reaction:



The SNCR process is also temperature-sensitive and, therefore, the effectiveness of  $\text{NO}_x$  removal depends on successful temperature control. In contrast to SCR technologies, no catalysts are required, which lowers the initial costs as well as the re-investment costs for catalyst replacement. Furthermore, energy costs may be lower, and less space is required.  $\text{NO}_x$  removal of about 50 percent is possible.

There are also several potential problems with the SNCR technique: The process can release ammonia; it also produces ammonium sulfate as a by-product, which can disrupt part of the system. The applicability of SCNR to coal units has not yet been demonstrated.

## **3.2 Mobile sources**

### **3.2.1 NO<sub>x</sub> control for Otto engines**

The formation of NO<sub>x</sub> in gasoline fueled Otto engines is determined by the combustion temperature, the residence time in the peak temperature zone and by the oxygen content of the fuel-to-air ratio (Figure 3.1).

Nowadays gasoline engines without emission controls are usually operated with stoichiometric or slightly over-stoichiometric fuel-to-air ratio, whereas engines built in the sixties were designed to operate below stoichiometry. The resulting high CO emissions of the early designs initiated the first technical regulations to limit CO emissions. The new engines indeed reduced the CO and VOC emissions, but at the same time (due to the higher stoichiometric ratio) the NO<sub>x</sub> emissions increased drastically.

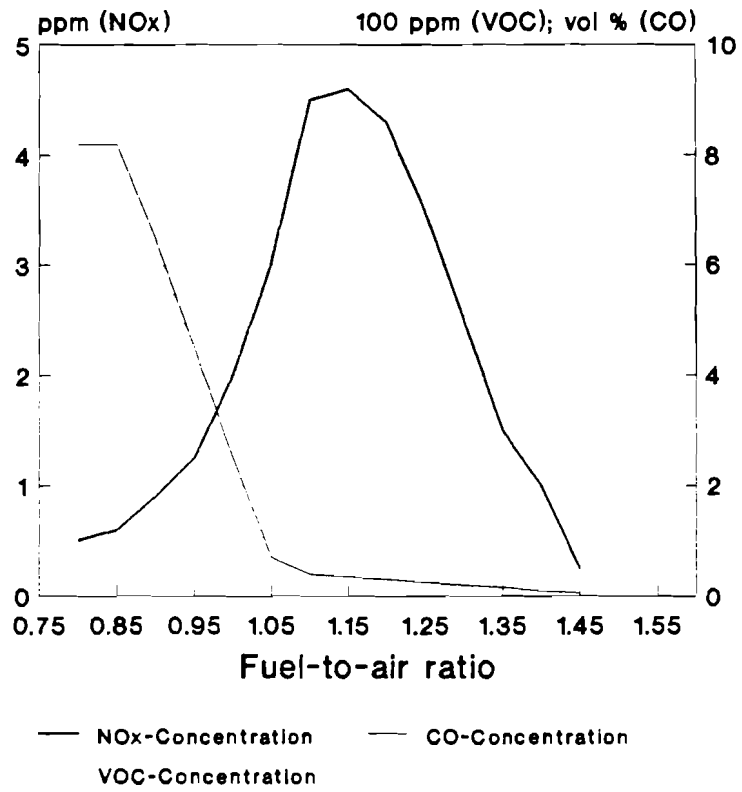
There are several means of reducing NO<sub>x</sub> emissions from gasoline fueled cars:

#### **Exhaust gas recirculation (EGR)**

The recirculation of exhaust gases substitutes part of the fresh intake air by exhaust gas, reducing the oxygen content in the combustion chamber and dampening the temperature peaks through its additional heat capacity. Both effects contribute to lower NO<sub>x</sub> emissions. Removal efficiencies of up to 30 percent are achievable without any increase in fuel consumption.

#### **Lean burn engines**

A change in the stoichiometry of the fuel-to-air ratio towards leaner mixtures also results in reduced NO<sub>x</sub> emissions. To guarantee satisfactory operation of the engines, some changes in the general design of the engines are necessary. Therefore, only new engines can be designed along the lean burn concept. The cars presently available with lean burn engines show satisfac-



Source: Umweltbundesamt 1989

Figure 3.1: Variation of emission levels with fuel-to-air ratio  $\lambda$  for an Otto-Cycle Engine

tory  $\text{NO}_x$  reduction for lower speed and comply with the ECE standards; at high speed, however, due to the high oxygen content of the exhaust gas their emissions may exceed those of conventional cars without control.

### **Catalytic reduction**

A catalytic converter enables and accelerates the chemical conversion of CO, VOCs and  $\text{NO}_x$  to  $\text{CO}_2$ ,  $\text{H}_2\text{O}$  and  $\text{N}_2$  at temperatures well below that at which it would occur spontaneously. The oxidation of CO and VOC is facilitated by completing the combustion process, nitrogen oxides are catalytically reduced. The catalysts consist of ceramic materials coated with precious metals (platinum, palladium or rhodium) or with active metal oxides (e.g. gamma alumina, copper oxide, etc.). Catalysts require the use of lead-free fuels, since the leaded antiknock additives form inorganic lead salts deposit on the catalytic surface, thereby deactivating it.

The **three-way catalytic** concept uses a single unit which oxidizes CO and VOC to carbon dioxide and reduces  $\text{NO}_x$  to nitrogen. For this process to work, it is necessary to have very careful control of the concentrations of all the gases on the catalytic surface. Therefore, these systems require a fuel injection system capable of maintaining precise control of the fuel-to-air ratios under all driving conditions. This is usually achieved by means of electronic fuel injection on 'feedback' carburettors combined with an oxygen sensor in the exhaust gas stream. The catalytic unit is programmed to control some 70 to 90 percent of the CO/VOC/ $\text{NO}_x$  during urban driving and up to 99 percent at high speed.

The **uncontrolled catalyst** does not control the fuel-to-air ratio and therefore does not require the fuel injection system and the oxygen sensor. Consequently, the catalyst works partly in the oxidizing mode (mainly reducing CO and VOCs) and partly in a  $\text{NO}_x$  reducing mode (lowering

NO<sub>x</sub>). The resulting NO<sub>x</sub> removal is lower than with controlled three way catalysts, but for smaller sized cars meets the requirements of the 'Luxembourg compromise' of the European Community.

There are also other catalytic systems available (e.g. the oxidation catalyst), but they do not have impacts on NO<sub>x</sub> emissions.

### **Two-stroke engines**

There are a large number of two-stroke operated vehicles in some Eastern European countries. These conventional engines produce a comparably large amount of CO and VOC emissions, but only low emissions of NO<sub>x</sub>. Since the production of these engines in Europe has been virtually stopped this year, no control options are considered. However, a 'stratified charge two-stroke' concept would enable drastic reduction of all three pollutants with CO and NO<sub>x</sub> rates below those of comparable four-stroke engines.

### **3.2.2 Diesel engines**

The high pressures and temperatures, and the relatively low fuel-to-air ratios in diesel engines reduce the incomplete combustion, making these engines more fuel efficient than spark-ignition engines. Due to the lower degree of incomplete combustion, diesel engines emit lower amounts of HC and CO than do Otto engines, whereas NO<sub>x</sub> emissions are the same or lower. Approximately 10 to 20 percent of nitrogen oxides from diesel engines are emitted as NO<sub>2</sub> (nitrogen dioxide), which is five times more toxic than NO (nitrogen monoxide). Gasoline engines emit less than 10 percent as NO<sub>2</sub>. However, in the atmosphere this NO converts to NO<sub>2</sub> within a short time.

For diesel engines there is also an inherent conflict between some of the most powerful NO<sub>x</sub> control techniques and the emissions of particulates. This 'tradeoff' is not absolute - various NO<sub>x</sub> control techniques have varying effects on soot and VOC emissions, and the importance of these effects varies

with engine speed and load. These tradeoffs place limits on the extent to which any one of the three pollutants can be reduced. At the moment there is no aftertreatment technique commercially available to reduce NO<sub>x</sub> emissions from diesel engines. The process of catalytic NO<sub>x</sub> reduction used on gasoline vehicles is inapplicable to diesel; because of their heterogeneous combustion process, diesel engines require substantial excess air, and their exhaust thus inherently contains significant oxygen. The three-way catalyst used on automobiles requires a precise stoichiometric mixture in the exhaust to properly function; in the presence of excess oxygen, their NO<sub>x</sub> conversion efficiency rapidly approaches zero.

A number of aftertreatment NO<sub>x</sub> reduction techniques which *will* work in an oxidizing exhaust stream are currently available or under development for stationary sources (e.g. Selective Catalytic Reduction SCR, Selective Non-Catalytic Reduction SNCR, etc.). However, each of these systems require a continuous supply of some reducing agent such as ammonia. Because of the need for frequent replenishment of this agent and the questions of crash safety, such systems are considered impractical for vehicular use.

#### **Diesel passenger cars**

Usually the design of the engines of diesel passenger cars use the indirect injection concept, in contrast to engines for heavy duty trucks, which are built as direct injection engines. The direct injection results typically in twice as high NO<sub>x</sub> emissions as the indirect injection design.

In a manner analogous to that for gasoline engines, combustion modifications (exhaust gas recirculation (EGR), delayed injection and staged combustion) can be used for the reduction of NO<sub>x</sub> emissions. EGR reduces the partial pressure for oxygen and the combustion temperature, leading to reduced NO<sub>x</sub> formation. Although for partial load emission reduction of some 20 to 30 percent is achievable, the strong increase of particulate matter generation limits the recirculation of the exhaust gases at full load.

## **Heavy Duty Trucks**

There is no single technology for drastically reducing NO<sub>x</sub> emissions from heavy duty trucks without major adverse impacts on the emissions of soot, VOC and noise, and on the fuel efficiency. However, some emission reductions can be achieved by the following measures:

**Injection Timing.** The timing relationship between the beginning of the fuel injection and the top of the compression stroke of the piston has an important effect on diesel engine emissions and fuel economy. For purposes of fuel efficiency it is preferable that the combustion begins just at the point of greatest compression, which requires fuel injection somewhat before this point. A long ignition delay provides more time for air and fuel to mix, which increases both the amount of fuel that burns in the premixed combustion phase and the maximum temperature in the cylinder. Both of these effects tend to increase NO<sub>x</sub> emissions, but reduce particulate and VOC emissions. Therefore, the injection timing must compromise between emissions of particulates and VOC and fuel economy on one hand and noise, NO<sub>x</sub> emissions and maximum cylinder pressure on the other. A higher injection pressure might alleviate the need for this compromise.

**Turbocharging and Intercooling.** A turbocharger consists of a centrifugal air compressor feeding the intake manifold, mounted on the same shaft as an exhaust gas turbine in the exhaust stream. By increasing the mass of air in the cylinder prior to compression, turbocharging correspondingly increases the amount of fuel that can be burned without excessive smoke, the potential maximum power output and the fuel efficiency of the engine. The compressed air can be cooled in an intercooler before it enters the cylinder. This increase of the air mass in the cylinder and the reduction of its temperature can reduce



both NO<sub>x</sub> and particulate emissions. In the U.S., virtually all engines will be equipped with these systems by 1991.

**Exhaust Gas Recirculation.** EGR is a time-proven NO<sub>x</sub> control technique for light-duty gasoline and diesel vehicles. In heavy-duty trucks, EGR has been shown to increase wear rates and oil contamination, resulting in higher maintenance expenses and shorter engine life (Cadmán and Johnson, 1986). It is also considered to have little advantage over other NO<sub>x</sub> control techniques such as retarding injection time. However, some recent research results suggest that a re-evaluation of this technique may be in order.

### 3.3 NO<sub>x</sub> control options selected for cost evaluation

Since the RAINS model can only deal with a limited number of control options for each combustion sector, the most important NO<sub>x</sub> reduction techniques were identified and costs evaluated. Within the model each control option is basically described by its abatement costs and removal efficiency. Thus these economic properties of the most common NO<sub>x</sub> abatement options also represent other techniques with the same cost-efficiency ratio, especially since these alternative methods have to compete on the market against the predominant techniques.

#### 3.3.1 Stationary sources

For stationary sources (powerplants, industry) two groups of NO<sub>x</sub> control options were selected:

**Combustion Modifications.** This group describes the control of NO<sub>x</sub> emissions by optimizing boiler design, applying 'Low-NO<sub>x</sub> burners'

and 'Off-stoichiometric combustion'. These options are available both for the construction of new plants and for retrofit application to existing units. An average  $\text{NO}_x$  removal efficiency of 30 percent is assumed to be achievable with these processes without impacts on CO and VOC emissions. Since the underlying design principles are already part of the general technical standards, it seems reasonable to assume that the planning of all new plants will automatically incorporate these construction guidelines. Advanced methods, such as catalytic combustion, are not considered in this analysis due to the lack of operating experience. If such a technology becomes available and proves to be commercially successful, the overall technical and economic performance would have to be equal or even better than those of conventional methods. For this reason, the procedure that we have selected has a tendency to overestimate future control costs.

**Flue Gas Cleaning.** The most common flue gas cleaning technique in Europe at present is Selective Catalytic Reduction (SCR) with an assumed average  $\text{NO}_x$  reduction of some 80 percent, in compliance with the U.S. standard of 1985. In theory there might be better control technologies than SCR, but, due to its dominating market position and the large construction and operating experience gained in Europe, it will be difficult for other methods to compete with the SCR process.

**Combined  $\text{NO}_x$  Control.** Because these two control options apply to different parts of the  $\text{NO}_x$  formation process, it is also possible to combine primary measures such as combustion modification and secondary options such as SCR. The resulting removal efficiency (compared to uncontrolled combustion) could reach 90 percent. Because of the lower  $\text{NO}_x$  concentration at the inlet of the SCR plant the consumption of reaction agents ( $\text{NH}_3$ ) will be reduced, resulting in lower operating

expenditures for the SCR unit.

### 3.3.2 Mobile sources

The data base for mobile sources comprises four categories:

- Gasoline fueled cars with four-stroke Otto engines
- Gasoline fueled cars with two-stroke Otto engines
- Diesel fueled passenger cars and light-duty trucks
- Diesel fueled heavy duty trucks

For gasoline fueled cars with **four-stroke engines** two levels of NO<sub>x</sub> control are considered:

- A moderate reduction, describing technical solutions to fulfill existing regulations such as the **EEC-Luxembourg compromise** for smaller cars. This involves several kinds of engine modifications (including EGR and the concept of the Lean Burn Engines) as well as the application of uncontrolled catalytic converters. The NO<sub>x</sub> reduction efficiency (compared to uncontrolled engines) lies typically around 50 percent. Due to the lack of sufficient operating experience in lean burn engines, the cost estimates for this degree of control is based on the costs of the uncontrolled catalyst. It is assumed that the emissions of CO and VOCs are also simultaneously reduced by 50 percent.
- More complex control concepts to comply with the **U.S. 1985 Standards**. These standards, which require an average reduction of at least 80 percent compared to the uncontrolled case, can currently be met by application of the three-way catalyst. Some countries have already adopted these regulations: USA, Canada, Japan, Austria, Finland, Norway, Switzerland and Sweden for the whole fleet and the EEC

countries for cars with cylinder volumes of more than 2 litres. Emissions of CO and VOC are simultaneously reduced to the same degree.

As mentioned above, because of the low importance of **two-stroke engines** in Western Europe and the low probability of retrofits for existing Eastern European cars, no NO<sub>x</sub> control is considered for this group of vehicles.

For **diesel passenger cars** a group of engine modifications is included to reduce their emissions by 30 percent. These reductions can be achieved by EGR, delayed injection and staged combustion.

Because of the importance of **Heavy Duty Trucks** for European NO<sub>x</sub> emissions, two levels of NO<sub>x</sub> control are specified. The uncontrolled status is based on the ECE guideline ECE.R49, which is comparable to pre-1988 U.S. Federal emission standards. This regulation represents a lowest common level of diesel engine technology worldwide, including a small retardation of the injection timing in order to reduce NO<sub>x</sub>, use of special injection nozzles to reduce HC and particulate matter, and some smoke control measures.

**U.S. 1988 Standards** This level of control is intended to reflect current (1988-1990) diesel engine technology in the U.S. While this level of technology is now required in the U.S., it is not unique to the U.S. and is already often applied in modern European trucks. The emissions of NO<sub>x</sub> are reduced by 25 percent (compared to the base case of the ECE.R49 regulation) with no impacts on VOCs, particulate matter and CO. The standards can be met via turbocharging with air-to-air or low-temperature air-water aftercooling. Further NO<sub>x</sub> control is provided by moderately retarded fuel injection at increased injection pressure. For the most part, this involves only incremental changes to the existing technology, rather than major redesign.

**U.S. 1991 Standards** This level of emission control reflects essentially the coming state-of-the-art in diesel engine technologies – those being de-

veloped in compliance with the U.S. 1991 emission standards. These standards represent roughly the feasibility for in-cylinder emission control alone (using currently available technology). The effect on NO<sub>x</sub> emissions is a 40 percent reduction, and can be achieved only by a complete redesign of large portions of the engine and combustion system. Besides the complete change of the in-chamber combustion conditions, NO<sub>x</sub> reductions are maximized through electronically controlled retardation of the fuel injection over most of the speed/load range and cooling the compressed air as much as possible. Through complex design guidelines, a simultaneous reduction by 50 percent for VOC and PM emissions can be achieved.

## Chapter 4

# Costs of NO<sub>x</sub> abatement

### 4.1 Principles of cost calculation

The intention of the approach in this report is to identify the values to society of the resources diverted in order to reduce NO<sub>x</sub> emissions in Europe. In practice, these values are approximated by estimating costs at the production level, rather than prices to the consumers. Therefore, any mark-ups charged over production costs by manufacturers or dealers do not represent actual resource use and are ignored. Certainly there will be transfers of money that have impacts on the distribution of income or on the competitiveness of the market, but these should be removed when considering the efficiency of resource allocation (see e.g. Transport Canada, 1986). Any taxes added to the production costs are similarly ignored as transfers.

The analysis will produce a framework to estimate these values in a consistent way for all European countries despite the differences between their economic systems. To eliminate the influence of these economic differences, a basic assumption was made of the existence of a free exchange of control technologies in Europe. Furthermore, it was assumed that on the competitive market technologies will be available for all countries at equal costs.

The results of the economic evaluation of NO<sub>x</sub> control options will not

predict costs for specific plants in individual countries, but will enable a general comparative analysis of different pollution control options for different countries, source categories and fuel types. The main objective of the approach, however, is the consistent international comparison of

- costs for different NO<sub>x</sub> abatement strategies, based on different energy scenarios; and
- a comparison of pollution control costs among countries.

The necessity to assess abatement costs for all countries in Europe limits the level of detail which can be maintained. Data availability and computational constraints require simplifications which might appear too approximate for studies focused on one country only. Therefore, the results of the economic evaluation should be considered more as indicative than as absolute cost estimates: the main emphasis is put on international consistency and comparability.

#### 4.1.1 International consistency

There are not only economic but also structural differences in national energy infrastructures, resulting in variations of the actual costs of the application of a given set of technologies. For example, the same type of an SCR unit with the same investment costs will reduce more NO<sub>x</sub> if installed in a powerplant running in a baseload mode than in a peak load mode. Consequently, the costs per abated ton of NO<sub>x</sub> will be greater in the latter case. In reality, the average capacity utilization as well as the boiler size distribution has a significant influence on the abatement costs in a country.

The second major influence on costs of national abatement strategies is the structure of energy consumption. Different source categories require different control efforts and costs. Not surprisingly, the costs necessary to achieve certain levels of emission reductions are directly related to the actual

potential for applying control options to certain source categories. Therefore, the characteristics of national energy systems (importance of coal use, share of the transport sector, etc.) produces major differences in potential and costs for emission reductions.

#### **4.1.2 Benefits of NO<sub>x</sub> control**

The final goal of each NO<sub>x</sub> control measure is the reduction of the adverse effects to human health, natural resources and manmade material of nitrogen deposition or concentration in the atmosphere. It is a major objective of the RAINS model to quantify such negative effects. However, at the moment the model does not express any benefits achieved by emission reductions in monetary terms, but restricts itself to the prediction of observable physical variables (such as pH values, areas of forest at risk, etc.). Therefore, the economic evaluation of NO<sub>x</sub> control excludes such benefits of emission reductions and concentrates purely on the abatement costs (resources) necessary to achieve the abatement.

Similarly also macroeconomic effects and potential benefits (e.g. impacts on the employment rate, trade balance, energy prices, crowding out of capital, etc.) are also excluded from this first analysis.

A difficult problem arises when control technologies for NO<sub>x</sub> simultaneously reduce (or possibly increase) the emissions of other air pollutants (e.g. the three-way catalytic converter also reduces CO and VOC). The overall economic evaluation of such techniques depends crucially on the value attributed to the emission reductions of these pollutants. If the control of NO<sub>x</sub> is selected as a single target, such control options may turn out as less cost efficient than other techniques (e.g. reducing just NO<sub>x</sub> at lower costs). On the other hand, if they are evaluated in an integrated context, where the reduction of other substances is also of interest, they may turn out to be extremely cost-efficient compared to a set of other measures necessary to



achieve the same improvements.

However, even if it would be the consensus that future policies have to consider several pollutants, the question of the relative importance of emission reductions for individual substances would still remain open. In principle, such tools as the RAINS model can be used to analyse the tradeoffs between different pollutants for specific problems (such as the acidification process in the environment) and thereby derive the relative importance of pollutants. However, in reality the problems are multi-faceted and, therefore, no simple solution seems available within the near future. This means that, for this analysis, the weighting of achieved emission reductions for different emission reductions remains open to subjective judgement.

## 4.2 Economic method

The method of cost estimation applied in this study uses standard methods of investment analysis applied to the question of emission abatement from a public policy perspective (Rentz, 1987). As explained above, a business perspective would very likely use these techniques in a slightly different way because of financial and profit considerations, which are not appropriate for public policy. Specifically, this difference of perspective would affect such parameters as discount rate, plant lifetime, financial outlays versus real resource costs, etc.

The objective of the abatement investment analysis is to calculate the *life cycle costs* of reducing emissions from individual source types and to relate these costs to the emission abatement achieved. Because costs are incurred, and revenues or benefits (e.g. abatement) are received at different points in time, it is necessary to choose one point in time for aggregation and comparison. A *present value* (PV) is the value that the flow of all costs or all benefits would have if they were accrued to today, or to a year zero. A *levelized* cost or emission reduction is the annual value that would have

to be paid or received each year over the lifetime of the abatement system to be equivalent to a given PV; that is, if the PV were evenly spread over the lifetime of the system.

To approximate the values of future costs or benefits to a present value the method of *discounting* is generally used. Interest rates are one form of discount rates determined by supply and demand (alternative uses) of money. So are *opportunity costs*. The appropriate discount rate to use for public policy analysis is very controversial and must consider several points:

- the cost of borrowing money;
- the 'opportunity costs' or the return that would be feasible by putting those resources to some other use, including returns that may not be valued by private markets (i.e. social benefits);
- subjective rate of time preference;
- consideration of future generations of people and resource bases.

For this analysis the use of a real discount rate (nominal discount rate – inflation rate) eliminates the difficulty of projecting future inflation.

## **4.3 Stationary sources**

### **4.3.1 The algorithm for the cost evaluation**

In order to calculate the life-cycle costs according to the investment analysis method it is necessary to differentiate the expenditures into

- investment costs,
- cost items depending on investments, and
- operating costs.

### Investment costs

The investment costs include the expenditure accumulated until the start-up of an installation, such as delivery of the installation, construction, civil works, ducting, engineering and consulting, licence fees, land requirement, working capital (e.g. stocks, process delays) etc. The model does not account for these cost items individually, but allows the use of aggregated investment functions.

The following description uses the indices  $i$ ,  $j$ ,  $k$  and  $l$  to indicate the nature of the parameters:

- $i$  denotes the fuel type
- $j$  the economic sector
- $k$  the control technology
- $l$  the country.

If there is a size dependency of the unit investment costs  $I_{i,j,k,l}$  (e.g. due to 'economics of scale'), it can be incorporated into the model by equation 4.1. The necessary size of an abatement installation for a certain plant capacity  $bs_i$  is determined by the fuel-specific flue gas volume  $v_i$  to be handled. The form of the function is described by its coefficients  $ci^f$  and  $ci^v$ . The more complicated situations arising for retrofit applications are taken into account by a retrofit cost factor  $r_k$ . Since the investment cost functions are usually scaled to output capacities of plants (e.g.  $MW_{el}$ ), the thermal efficiency of the combustion process  $eff_{i,j,l}$  is used to relate the costs to fuel input.

$$I_{i,j,k,l} = (ci_k^f + \frac{ci_k^v}{bs_{i,j,l}}) v_i / r_k \text{ eff}_{i,j,l} \quad (4.1)$$

The investment cost functions describe only the costs for construction of the equipment, and exclude the costs for the catalytic material. Since these

costs depend on the actual operation of the plant, they will be accounted for under the cost item 'variable operating costs'.

The investments are annualized over the plant lifetime  $lt_{j,k}$ , using the interest rate  $q_l$  (equation 4.2).

$$I_{i,j,k,l}^{an} = I_{i,j,k,l} \frac{q_l^{lt_{j,k}} (q_l - 1)}{q_l^{lt_{j,k}} - 1} \quad (4.2)$$

### Investment related costs

The annual fixed expenditures  $OM^{fix}$  cover the costs of maintenance, taxes and administrative overhead. These cost items are not related to the actual use of the plant. In contrast to desulfurization plants, no additional labor requirements are reported for  $NO_x$  control equipment, because the operation of the devices is automatically controlled to a high degree. As a rough estimate for the annual fixed expenditures, most technical standards use a standard percentage  $f_k$  of the total investments costs:

$$OM_{i,j,k,l}^{fix} = I_{i,j,k,l} f_k \quad (4.3)$$

### Operating costs

The variable operating costs  $OM^{var}$  related to the actual operation of the plant take into account the costs for the increased energy demand for operating the device (e.g. for the fans and for reheating) and for sorbent material (e.g.  $NH_3$ ). These cost items are calculated based on the specific demand  $\lambda^x$  of a certain control technology and its (country-specific) price  $c^x$ .

$$OM_{i,j,k,l}^{var} = \lambda_k^e c_l^e + nox_{i,j,k} x_{i,j,k} \lambda_k^s c_l^s \quad (4.4)$$

$\lambda^e$	additional energy demand
$\lambda^s$	sorbents demand
$c^s$	sorbents price
$c^e$	energy price
$nox_{i,j,k}$	NO <sub>x</sub> emission factor
$x_{i,j,k}$	removal efficiency

If a control technology makes use of catalysts, the periodical replacement costs for this equipment (depending on the real operation time of the plant) is also included in this cost category:

$$OM_{i,j,k,l}^{cat} = \lambda_{i,j}^{cat} v_i eff_{i,j} ci^{cat} pf_{i,j,l} / lt_k^{cat} \quad (4.5)$$

$\lambda^{cat}$	catalyst volume
$ci^{cat}$	costs of catalysts
$pf_{i,j,l}$	operating time
$lt^{cat}$	lifetime of catalysts.

#### Unit costs of NO<sub>x</sub> control

Based on the above mentioned cost items, the unit costs for the removal of NO<sub>x</sub> emissions can be calculated. In Equation 4.6 all expenditures of a control technology are related to one unit of fuel input  $ce_{i,j,k,l}$ . The investment related costs are converted to fuel input by applying the capacity utilization factor  $pf_{i,j,l}$ :

$$ce_{i,j,k,l} = \frac{I_{i,j,k,l}^{an} + OM_{i,j,k,l}^{fix}}{pf_{i,j,l}} + OM_{i,j,k,l}^{var} + OM_{i,j,k,l}^{cat} \quad (4.6)$$

Although this cost coefficient  $ce_{i,j,k,l}$  is useful for the calculation of price effects on the electricity price, the cost efficiency of different control options can only be evaluated by relating the abatement costs to the amount of

reduced NO<sub>x</sub> emissions. However, at this point, the question, of how simultaneous reductions of emissions other than NO<sub>x</sub> should be credited becomes crucial. As can be seen in Equation 4.8, the overall figure of cost efficiency  $cn'_{i,j,k,l}$  is extremely sensitive to the relative weight factors  $f^{NOx}$ ,  $f^{CO}$  and  $f^{VOC}$ :

$$cn_{i,j,k,l} = \frac{ce_{i,j,k,l}}{nox_{i,j} x_k} \quad (4.7)$$

$$cn'_{i,j,k,l} = \frac{ce_{i,j,k,l}}{nox_{i,j} x_k^{NOx} f^{NOx} + voc_{i,j} x_k^{VOC} f^{VOC} + co_{i,j} x_k^{CO} f^{CO}} \quad (4.8)$$

### 4.3.2 Data for cost calculation

#### Types of data

The RAINS model uses two groups of parameters for the above cost calculation routine:

- **Technology-specific data** describe the typical economic and technical properties of control technologies and are assumed to be equal for all countries under consideration. This group comprises the *technical* parameters (removal efficiency, technical lifetime, requirements for energy and sorbents material, and the *economic* parameters of the investment cost functions, the costs of catalysts, additional expenditures for retrofit installations and maintenance costs.
- **Country-specific data** describe the specific conditions in individual countries under which abatement technologies have to be applied. The most important parameters are the average capacity utilization of plants, the average boiler size, interest rates and the prices for energy and material consumption (see Table 4.1).

Table 4.1: Parameters used in the cost calculation routine

<b>Technology-specific parameters</b>	
$ci^f, ci^v$	parameters for investment cost function
$ci^{cat}$	costs of catalysts
$f_k$	annual maintenance costs
$lt_{j,k}$	lifetime of installation
$lt_k^{cat}$	lifetime of catalyst
$x_k$	NO <sub>x</sub> removal efficiency
$\lambda_k^e$	additional energy demand
$\lambda_k^s$	material consumption
<b>Country-specific parameters</b>	
$pf_{i,j,k}$	capacity utilization
$bs_{i,j,k}$	average boiler size
$q_l$	interest rate
$c_l^e$	energy(electricity) price
$c_l^s$	price for sorbents (e.g. NH <sub>3</sub> )

### Data sources

Since there is already a large amount of experience in NO<sub>x</sub> control in some European countries, the RAINS model uses primarily European data and, to a lesser extent, North American and Japanese sources. Recently data have become available which are based on surveys of real expenditures (Jung, 1988; Schärer and Haug, 1987; OECD, 1988; Leggett and Corfee, 1987). A comparison of data from FRG, e.g. with that from the Netherlands shows good agreement for all major control technologies (Schärer and Haug, 1988; Okken 1988). They are assumed to be fairly representative for all of Europe and were therefore adopted in the RAINS model.

The country-specific data were compiled by IIASA and are based – as far as possible – on international statistics: Average boiler sizes and national capacity utilization is based on OECD/IEA statistics (e.g. OECD, 1989b). The costs of the increased energy consumption caused by flue gas cleaning devices are based on national electricity prices for industrial consumers (losses of income if electricity cannot be sold). For IEA countries, statistical material is available from IEA (OECD, 1989c). Due to the lack of a valid conversion rate for non-convertible currencies for Eastern European countries the revenues for electricity exports to Western countries are taken as opportunity costs for increased losses during power generation. Although the model provides the possibility of applying country-specific interest rates, for reasons of international consistency and equity a flat rate of 4 percent is used for all of Europe. In the same way, the world market price for ammonia is used as input price for all national economies. Tables 4.2 to 4.5 give an overview on the data used for the calculations:



Table 4.2: Technology-specific data for stationary sources

Parameter		CM	SCR	CM + SCR	Units
NO <sub>x</sub> removal efficiency	$x_k$	50	80	90	%
VOC removal efficiency	$x'_k$	0	0	0	%
CO removal efficiency	$x''_k$	0	0	0	%
lifetime in powerplants	$lt_{j,k}$	30	30	30	years
lifetime in industry	$lt_{j,k}$	20	20	20	years
coefficients for the investment function	$ci_k^f$	20	41	61	
	$ci_k^v$	5834	5834	5834	
cost of catalysts	$ci_k^{cat}$	-	40000	40000	DM/m <sup>3</sup>
lifetime of catalyst	$lt_k^{cat}$	-	12000	12000	hours
annual maintenance and overhead	$f_k$	0	6	6	% of total investments
NH <sub>3</sub> consumption	$\lambda_k^s$	0	250.	111.	kg / t NO <sub>x</sub>
additional energy consumption	$\lambda_k^e$	0	2	2	%

CM Combustion Modification

SCR Selective Catalytic Reduction

Table 4.3: Capacity utilization for powerplants (in hours per year)

<i>Country</i>	<i>Brown Coal</i>	<i>Hard Coal</i>	<i>Heavy Fuel Oil, Natural Gas</i>
Albania	4000	4000	4000
Austria	3504	3504	3066
Belgium	n.a.	3416	3679
Bulgaria	4818	4818	4380
CSSR	4818	4818	3153
Denmark	n.a.	3592	526
Finland	n.a.	2365	3854
France	3767	3767	1489
FRG	6745	4205	1226
GDR	4818	4818	2716
Greece	6132	4000	3504
Hungary	4292	4292	4292
Ireland	n.a.	3592	3416
Italy	3679	4030	4030
Luxembourg	n.a.	3504	3504
Netherlands	n.a.	3154	3942
Norway	n.a.	n.a.	964
Poland	4380	4468	4468
Portugal	4000	4117	4117
Romania	4380	4380	4380
Spain	4730	4468	4468
Sweden	n.a.	4000	1314
Switzerland	n.a.	n.a.	1401
Turkey	4993	2978	2978
UK	n.a.	4468	876
USSR	5168	5168	5168
Yugoslavia	4380	1927	1927

Table 4.4: Average boiler size for powerplants (in  $MW_{el}$ )

Country	Brown Coal	Hard Coal	Heavy Fuel Oil, Natural Gas
Albania	210	210	210
Austria	139	220	128
Belgium	n.a.	160	158
Bulgaria	210	210	210
CSSR	210	210	210
Denmark	n.a.	178	201
Finland	n.a.	134	82
France	202	252	306
FRG	235	206	190
GDR	210	210	210
Greece	243	210	155
Hungary	210	210	210
Ireland	n.a.	300	106
Italy	153	335	227
Luxembourg	n.a.	210	210
Netherlands	n.a.	328	193
Norway	n.a.	n.a.	210
Poland	210	210	210
Portugal	210	300	150
Romania	210	210	210
Spain	257	254	195
Sweden	n.a.	502	203
Switzerland	n.a.	210	150
Turkey	195	150	126
UK	n.a.	245	291
USSR	210	210	210
Yugoslavia	99	370	149

Table 4.5: Electricity price, real interest rate and NH<sub>3</sub> prices in Europe

<i>Country</i>	<i>Electricity Price DM/MWh</i>	<i>Interest Rate %</i>	<i>NH<sub>3</sub> Costs DM/t NH<sub>3</sub></i>
Albania	88	4.0	700
Austria	125	4.0	700
Belgium	97	4.0	700
Bulgaria	88	4.0	700
CSSR	88	4.0	700
Denmark	102	4.0	700
Finland	95	4.0	700
France	82	4.0	700
FRG	147	4.0	700
GDR	88	4.0	700
Greece	125	4.0	700
Hungary	88	4.0	700
Ireland	145	4.0	700
Italy	124	4.0	700
Luxembourg	114	4.0	700
Netherlands	86	4.0	700
Norway	31	4.0	700
Poland	88	4.0	700
Portugal	162	4.0	700
Romania	88	4.0	700
Spain	108	4.0	700
Sweden	88	4.0	700
Switzerland	142	4.0	700
Turkey	87	4.0	700
UK	126	4.0	700
USSR	88	4.0	700
Yugoslavia	88	4.0	700

## 4.4 Mobile sources

The cost evaluation for mobile sources follows the same basic approach as for stationary sources; however, due to structural differences slight modifications were necessary.

### 4.4.1 The algorithm for the cost evaluation

All costs and emission reductions are summed up over the whole lifecycle of the vehicles: The amount of abated  $\text{NO}_x$  emissions is calculated based on the emission factor for unabated emissions  $nox_{i,j}$ , the removal efficiency of the control option  $x_k$ , the average annual fuel consumption  $fuel_{i,j,l}$  of a vehicle and its lifetime  $lt_{i,j}$ :

$$rnox_{i,j,k,l} = nox_{i,j} x_k^{NOx} fuel_{i,j,l} lt_{i,j} \quad (4.9)$$

The same calculations can be performed for the abatement of VOC and CO:

$$rvoc_{i,j,k,l} = voc_{i,j} x_k^{VOC} fuel_{i,j,l} lt_{i,j} \quad (4.10)$$

$$rco_{i,j,k,l} = co_{i,j} x_k^{CO} fuel_{i,j,l} lt_{i,j} \quad (4.11)$$

The costs of applying control devices include the additional investments  $ci_{i,j,k}^f$ , increased maintenance costs  $f_k$  and the costs of potential replacements of parts of the control systems after its lifetime  $lt^{cat}$ :

$$OM_{i,j,k} = ci_{i,j,k}^f + (lt_{i,j,k} - 1)f_k + ci_{i,j,k}^f \frac{lt_{i,j}}{lt_{i,j}^{cat}} \quad (4.12)$$

Any (positive or negative) influence on fuel consumption is taken into account by:

$$OM_{i,j,k,l}^e = \lambda_{i,j,k}^e fuel_{i,j,l} c_{i,j,k,l}^e lt_{i,j} \quad (4.13)$$

The unit costs of abatement  $ce$  (related to one unit of fuel input) add up to

$$ce_{i,j,k,l} = \frac{OM_{i,j,k} + OM_{i,j,k,l}^c}{fuel_{i,j,k,l} lt_{i,j}} \quad (4.14)$$

If these costs are related to achieved emission reductions, again a measure for the cost efficiency of the control option will be obtained ( $f^x$  are the relative weights for the individual pollutants):

$$cn_{i,j,k,l} = \frac{ce_{i,j,k,l}}{rnox_{i,j} f^{NOx} + rvoc_{i,j} f^{VOC} + rco_{i,j} f^{CO}} \quad (4.15)$$

It should be mentioned that, in the present form, the factors leading to differences among countries are the annual energy consumption per vehicle and the fuel prices for the additional energy consumption. In reality, the average emission factors may also differ among countries according to the fleet composition and typical driving cycles. However, at the present time it does not seem feasible to obtain reliable data with respect to this item.

#### 4.4.2 Data for cost calculation

In analogy to stationary sources international surveys on costs of pollution control equipment was the preferred data source for the RAINS model. Therefore, technology-specific data rely mainly on OECD surveys (OECD, 1988a; OECD, 1988b) and UN-ECE (1988a), and were modified to the specific requirements (Table 4.6) and (Table 4.7).

Table 4.6: Technology-specific data for mobile sources

Parameter		Heavy Duty Trucks		Gasoline Vehicles		Unit
		U.S. 1988	U.S. 1991	EEC-compr.	U.S. 1985	
NO <sub>x</sub> removal efficiency	$x_k$	25	40	50	90	%
VOC removal efficiency	$x'_k$	0	0	50	90	%
CO removal efficiency	$x''_k$	0	0	50	90	%
lifetime of vehicles	$lt_{j,k}$	10	10	10	10	years
investment costs	$ci^f$	1200	2200	800	1000	DM/car
lifetime of catalyst	$lt_k^{cat}$	n.a.	n.a.	10	10	years
annual maintenance and overhead	$f_k$	10	15	0	0	% of total investm.
additional fuel consumption	$\lambda_k^e$	3	8	1.5	- 1.5	%

Table 4.7: Fuel prices (without taxes) and annual fuel consumption of mobile sources

<i>Country</i>	<i>Fuel price</i>		<i>Fuel consumption</i>	
	<i>Diesel</i>	<i>Gasoline</i>	<i>Diesel</i>	<i>Gasoline</i>
	<i>[DM/MJ]</i>		<i>[GJ/car/year]</i>	
Albania	10.90	12.85	400.	45.
Austria	12.85	13.99	790.	49.
Belgium	9.69	12.38	650.	45.
Bulgaria	10.90	12.85	400.	81.
CSSR	10.90	12.85	310.	30.
Denmark	11.82	11.63	520.	44.
Finland	13.47	19.16	780.	44.
France	9.32	9.37	840.	35.
FRG	8.77	10.80	640.	47.
GDR	10.90	12.85	150.	41.
Greece	7.11	8.92	390.	62.
Hungary	10.90	12.85	320.	49.
Ireland	13.22	13.04	600.	65.
Italy	9.88	11.81	600.	31.
Luxembourg	9.48	12.25	810.	49.
Netherlands	10.08	12.44	910.	43.
Norway	11.32	13.25	280.	45.
Poland	10.90	12.85	260.	35.
Portugal	11.42	13.59	840.	28.
Romania	10.90	12.85	400.	45.
Spain	9.88	11.19	490.	33.
Sweden	13.66	13.87	630.	55.
Switzerland	10.95	12.16	260.	52.
Turkey	13.14	20.51	400.	45.
UK	10.68	11.02	440.	54.
USSR	10.90	12.85	510.	58.
Yugoslavia	10.90	12.85	380.	31.



## 4.5 Cost coefficients for NO<sub>x</sub> abatement

Using the parameters as presented in section 4.3.2, the evaluation of Equations 4.1 to 4.8 can be performed for all NO<sub>x</sub> control options under consideration. Due to limited space, this paper will only list the abatement costs for the most important control options. However, a complete listing can be obtained by model runs.

If costs are related to electricity production, for SCR at new power stations using brown coal they vary between 0.69 and 0.95 DPf/kWh. The costs of SCR for new boilers using hard coal increase the costs of electricity generation between 0.55 and 0.82 Dpf/kWh. These estimates show good agreement with other published sources (e.g. Schärer and Haug, 1988). If these costs are related to the amount of NO<sub>x</sub> removed, costs range for brown coal plants from 2.83 to 3.87 DM/kg NO<sub>x</sub> and for hard coal stations from 2.04 to 3.04 DM/kg NO<sub>x</sub> (Table 4.8). These ranges in costs are caused by national differences in boiler size distributions and capacity utilization.

Introduction of the U.S. 1991 standard for heavy duty trucks would require costs in a range between 3.74 and 14.93 DM/kg NO<sub>x</sub> (Table 4.9).

For the evaluation of the controlled three-way catalyst, the credit for simultaneous reductions of VOC and CO becomes of crucial importance. If no credit is given to the reduction of other pollutants, this technology is one of the more expensive options of controlling NO<sub>x</sub> (with costs in a range between 3.72 and 10.58 DM/kg NO<sub>x</sub>). However, if the side effects are also taken into account, it appears to be a very cost efficient solution (between 0.47 and 1.32 DM/kg of abated pollutant, if NO<sub>x</sub>, VOC and CO are weighted equally).

The considerable variations in control costs of mobile sources among countries are caused by two factors:

- Differences in fuel prices (even if taxes are excluded).

Table 4.8: Costs of SCR for new brown coal (BC) and hard coal (HC) powerplants (PP) per kWh produced electricity and per kg NO<sub>x</sub> removed

Country	SCR, new BC PP		SCR, new HC PP	
	DPf/kWh	DM/kg NO <sub>x</sub>	DPf/kWh	DPf/kg NO <sub>x</sub>
Albania	0.80	3.31	0.59	2.18
Austria	0.87	3.87	0.63	2.33
Belgium	0.94	3.33	0.66	2.44
Bulgaria	0.75	3.09	0.55	2.04
CSSR	0.75	3.09	0.55	2.04
Denmark	n.a.	n.a.	0.64	2.35
Finland	n.a.	n.a.	0.82	3.04
France	0.83	3.41	0.58	2.16
FRG	0.69	2.83	0.60	2.23
GDR	0.75	3.09	0.55	2.04
Greece	0.70	2.86	0.60	2.23
Hungary	0.78	3.22	0.57	2.12
Ireland	n.a.	n.a.	0.61	2.24
Italy	0.90	3.70	0.57	2.10
Luxembourg	n.a.	n.a.	0.63	2.33
Netherlands	n.a.	n.a.	0.61	2.33
Norway	n.a.	n.a.	n.a.	n.a.
Poland	0.78	3.20	0.57	2.10
Portugal	0.83	3.43	0.59	2.17
Romania	0.78	3.20	0.57	2.11
Spain	0.74	3.06	0.56	2.07
Sweden	n.a.	n.a.	0.53	1.97
Switzerland	n.a.	n.a.	0.61	2.25
Turkey	0.75	3.08	0.71	2.62
UK	n.a.	n.a.	0.57	2.11
USSR	0.73	3.01	0.54	2.00
Yugoslavia	0.91	3.74	0.74	2.74

- Differences in annual fuel consumption per car. As listed in table 4.9, major variations of this variable exist for Europe.

Due to the limited accuracy of the underlying statistics (especially on the number of registered vehicles in Europe, including off-road vehicles), the magnitude of the observed variations could be questioned. Nevertheless it seems reasonable to introduce such differences rather than ignore them.

## 4.6 National cost curves for NO<sub>x</sub> abatement

As demonstrated above, national circumstances result in variations of the costs for applying the same control technology over Europe. However, these differences are not the only ones causing different costs of abatement strategies. Another source of variations is related to the structural differences of national energy systems which determine the potential for application of individual control options. One way to analyse the combined effect of these two factors is the compilation of 'national cost curves' for NO<sub>x</sub> abatement. These curves display the lowest costs for achieving varying reduction levels, applying the cost optimal combination of abatement options. In theory, they can be identified by repeated cost-optimization runs stepwise, changing overall reduction levels. A faster method, however, will rank the available control options according to their marginal costs for NO<sub>x</sub> reduction and link their individual potentials for emission removal.

Because the overall potential of reducing emission from a specified source has to be consistent, special provisions have to be taken for control options excluding each other (e.g. the uncontrolled catalysts and the controlled three-way system for mobile sources). In these cases, the marginal costs to be taken into account for the more expensive but also more efficient control option have to be related to the incremental emission reductions compared to the cheaper option.

Table 4.9: Costs of introducing U.S. Norm 1991 for heavy duty trucks and for 3-way catalysts for gasoline fueled cars (per kg of NO<sub>x</sub> abated)

Country	U.S. Standard 1991 DM/kg NO <sub>x</sub>	3-way catalyst	
		DM/kg NO <sub>x</sub>	DM/kg NO <sub>x</sub>
		<i>no credit</i>	<i>credit for</i>
		<i>for VOC and CO</i>	<i>VOC and CO</i>
Albania	6.65	6.69	0.87
Austria	4.49	5.74	0.72
Belgium	4.55	6.31	0.79
Bulgaria	6.65	3.72	0.47
CSSR	8.09	10.58	1.32
Denmark	5.64	6.48	0.81
Finland	4.62	6.31	0.79
France	3.80	8.26	1.03
FRG	4.46	6.06	0.76
GDR	14.93	7.66	0.96
Greece	6.19	4.58	0.57
Hungary	7.89	6.35	0.80
Ireland	5.35	4.27	0.54
Italy	4.83	9.30	1.16
Luxembourg	3.91	5.77	0.72
Netherlands	3.74	6.61	0.82
Norway	8.84	6.29	0.79
Poland	9.32	9.02	1.13
Portugal	4.12	10.28	1.29
Romania	6.65	6.95	0.87
Spain	5.58	8.73	1.09
Sweden	5.26	5.08	0.64
Switzerland	9.33	5.43	0.68
Turkey	6.99	6.13	0.77
UK	6.16	5.24	0.66
USSR	5.58	5.32	0.67
Yugoslavia	6.91	10.23	1.29

This formally correct and mathematically necessary procedure has important effects for the compilation of national cost curves. In the event that exclusive control options with different costs and removal rates exist for a source, the ranking procedure will consider the incremental marginal costs for the more expensive technology, which are greater than the original unit costs of abatement for this option. Therefore, the introduction of such control options will have less priority compared to a situation where the less efficient options would not have been introduced at all.

Again, this effect is of relevance for evaluation of the three-way catalyst. If no credit is given for simultaneous reductions of VOC and CO, in some countries the additional NO<sub>x</sub> removals of the three-way system (over the reduction achievable by uncontrolled catalysts) are very expensive. The three-way system is therefore ranked into the very expensive group of options. If, on the other hand, the uncontrolled catalyst would not have been considered in the procedure, the introduction of the three-way system would have lower unit and marginal costs and would therefore be ranked higher.

The Appendix contains cost curves of NO<sub>x</sub> reduction for all European countries, if the official forecasts of energy consumption for the year 2000 are taken as a basis. The two curves describe marginal and total costs of abatement. For these examples, no credit is given to simultaneous reduction of CO and VOC.

#### **4.7 Current reduction plans and maximum feasible reductions**

The data can also be used to analyse the control cost which are implied by the Sofia Protocol on NO<sub>x</sub> emissions (UN-ECE, 1988a). Although countries may, according to the protocol, select any year between 1980 and 1987 as their reference year for NO<sub>x</sub> reductions, due to lack of information 1980 was taken as the reference year. The aim of the protocol is to reach the

Table 4.10: Assumption of 'Best Available Technologies' in different economic sectors

Sector	Best Available Technology	Removal Efficiency
Powerplants	Combustion Modification + SCR	90 %
Industry	Combustion Modification + SCR Processes	90 %
Refineries	Combustion Modification + SCR Processes	90 %
Heavy Duty Trucks	U.S.-Standard 1991	40 %
Gasoline Cars	3-way catalyst	80 %
Industrial Process Emissions	Different Methods	80 %

specified levels by 1994; for reasons of comparability the projected energy consumption of the year 2000 was selected as the basis for the cost evaluation. Although 12 countries committed a 30 percent reduction and 8 others a standstill by 1994, the total European NO<sub>x</sub> emissions can be expected to decline by only 5 percent, because countries with high expectations on economic growth (mainly in Southern Europe) will increase emissions to balance out some of the reductions. Table 4.11 displays the emissions after implementation of the currently committed control measures.

The maximum technically feasible reductions apply the most efficient control technologies without changing the energy consumption itself (e.g. by energy conservation, fuel substitution, speed limits). For this scenario, the assumptions shown in Table 4.10 were made.

Table 4.11: NO<sub>x</sub> emissions (in kt NO<sub>x</sub>/year) after implementation of the Current Reduction Plans and the Maximum Technically Feasible Reductions.

Country	Current Reduction Plans		Maximum Feasible Reductions	
	kt NO <sub>x</sub>	% Reduction	kt NO <sub>x</sub>	% Reduction
Albania	46	+64	16	43
Austria	167	30	103	57
Belgium	307	30	181	59
Bulgaria	357	0	198	45
CSSR	628	0	214	73
Denmark	175	30	85	66
Finland	163	30	121	49
France	1360	30	674	66
FRG	2023	30	953	67
GDR	850	0	252	70
Greece	435	+82	132	45
Hungary	252	18	110	46
Ireland	117	+31	37	58
Italy	1020	30	678	55
Luxembourg	22	30	16	49
Netherlands	403	30	229	60
Norway	118	30	87	49
Poland	1597	0	551	65
Portugal	255	51	88	40
Romania	851	+29	335	50
Spain	950	0	538	44
Sweden	233	30	142	58
Switzerland	130	30	61	67
Turkey	1040	+192	514	+44
UK	2324	0	838	64
USSR	9454	0	3678	61
Yugoslavia	574	+45	184	53
Total	25854	5	11027	60

Table 4.12 lists the costs of achieving the specified emission levels of Table 4.11. Following the protocol, countries have committed emission reductions without specifying how they will attain these targets. Therefore, the cost estimate for the current reduction plans could only be based on the assumption of a cost optimal combination of reduction measures as computed by the national cost curves. However, in reality countries could also achieve these reductions by sub-optimal combinations, resulting in higher costs.

According to this estimate, the total European cost implied by the current reduction plans would amount to 4.5 billion DM/year. This is roughly 40 percent of the expenditures necessary to reach the sulfur reductions currently committed. However, the maximum technically feasible reduction of  $\text{NO}_x$  resulting in an overall emission decline of 60 percent would cost 66.3 billion DM/year.



Table 4.12: Abatement costs (in million DM/year) for the Current Reduction Plans (CRP) and the Maximum Technically Feasible Reductions (MFR)

	CRP 10 <sup>6</sup> DM/year	MFR 10 <sup>6</sup> DM/year
Albania	0	106
Austria	71	436
Belgium	114	888
Bulgaria	158	1291
CSSR	0	1703
Denmark	79	706
Finland	249	637
France	481	2651
FRG	523	5509
GDR	0	2691
Greece	0	924
Hungary	0	646
Ireland	0	193
Italy	1316	3606
Luxembourg	9	31
Netherlands	135	1054
Norway	169	512
Poland	0	3922
Portugal	0	508
Romania	0	2276
Spain	553	3116
Sweden	91	535
Switzerland	53	279
Turkey	0	2357
UK	256	5289
USSR	316	22468
Yugoslavia	0	2023
Total	4578	66371

## Chapter 5

# Conclusions

Several factors cause variations in the potential and costs for control of  $\text{NO}_x$  emissions among European countries. Based on an European emission inventory for nitrogen oxides, these differences can be explored and analyzed. The emission inventory computes anthropogenic  $\text{NO}_x$  emissions from energy combustion and industrial activities based on common emission factors for 8 fuel types and 5 combustion sectors.

A variety of options for control of  $\text{NO}_x$  emissions is presently available. However, this economic analysis is restricted to the most important methods which do not require structural changes in energy consumption. For stationary sources, combustion modifications and selective catalytic reduction (SCR) are used.  $\text{NO}_x$  emissions from heavy duty trucks can be reduced by two stages of reduction measures complying with the U.S. Norm 1988 and 1991. For gasoline cars, the use of controlled and uncontrolled catalysts is considered.

Several factors create variations of control costs among countries. Besides the structural differences in energy consumption for stationary sources, the annual capacity utilization and the average boiler size have the greatest influence on actual abatement costs. For the same control technology,

typical variations up to 20 percent can be expected.

The control costs for mobile sources are sensitive to the average fuel consumption (as a surrogate for the size composition of the fleet and the mileage driven) and national differences in fuel price. The resulting variations are larger for mobile sources than for stationary sources; however, at present some uncertainty about the accuracy of the underlying statistical material cannot be completely eliminated.

The cost efficiency of some control options is crucially related to the credit given to simultaneous removal of pollutants other than  $\text{NO}_x$ . If  $\text{NO}_x$  removal is considered separately, such abatement technologies appear to be relatively expensive. However, in an integrated context, if all pollutants are taken into account, they become extremely cost efficient. Since at the present time no general guideline on how to weight different substances has been accepted, no final evaluation can be performed yet.

An analysis of the currently committed reductions of  $\text{NO}_x$  emissions results in an expected decline of 5 percent over the whole of Europe. If countries would follow a pure cost minimizing principle, the involved annual expenditures can be estimated to be 4.5 billion DM per year. This amounts to roughly 40 percent of the costs for sulfur reductions presently announced. A maximum technically feasible reduction could reduce the European  $\text{NO}_x$  emissions by some 60 percent. The incurred costs would increase to 66 billion DM/year.

The analysis of international potential and costs for  $\text{NO}_x$  abatement opens the possibility of evaluating the cost efficiency of different control strategies. Furthermore, the analysis also provides an important input for designing receptor-oriented control strategies that allocate emission reductions spatially to attain prespecified regional deposition levels for nitrogen in cost optimal ways. However, an integrated analysis should also consider the contribution of ammonia to total nitrogen deposition.

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# APPENDIX

The appendix contains national cost curves for the abatement of  $\text{NO}_x$  emissions in Europe. These calculations are based on the forecast energy consumption of the year 2000 and exclude energy conservation and fuel substitution. In this example case, no credit is given to simultaneous reduction of other pollutants such as CO and VOC.

